Loopshaping Design Example





Pertormance Specifications Clused - loop stubility Loop crossover Frequency new I rad Kec

Tracking Performance :
 15(j0.01) \$ 0,0004
 15(j0.1) \$ 0,004
 15(j0.1) \$ 0,04
 15(j0.2) \$ 0,2

Jes) is the transfer function from rate. These bounds ensure that the error amplitude is small if r is a low frequency sinsusoid.

Noise Rejection:
 | T(j100) | ≤ 0,0004
 | T(j10) | ≤ 0,004
 | T(j10) | ≤ 0,04
 | T(j3) | ≤ 0,3

The is the transfer huncher from -n→X. These bounds ensure that high frequency noise has min small impact on the output.

We'll use loopshaping to design a Controller that Meets these specifications. Note that we're starting from Grequency domain specifications on S and T. Part of the design work is to actually figure out what specifications on S and T are reasonable, you'll have some practice doing this on the borework.

Step 1 Translate specs on 5 and T into specs on 12 the bup transfer function L=GK. a) Bounds on JG) = 1+GG) K(G) = 1+LG) IF we have an bound: |SGW) = / 1/1/1/15 b They we need: 11+ L(1w) 7 1/6 (this is equivalent) 1f | L (jw) | ≥ 1 +1 then | 1+ L(jw) | = |L(jw)|-1 = 1/8 This Follows from the triangle inequality: lats 1 \$ lal + 161 Specifically $|L(yw)| = |L(yw)+1-1| \le |L(yw)+1| + |-1|$ ET => 16/001 - 15 1600++1 1 L (jw) 1 7 1+16 => /S(w)/5b Upper Bound on Lower Bound w 15(w) on ILGNUI - If the bound on ISGW) 1 0.01 0,0004 2501 0.04 0,1 is back they the bound 26 on 166wall is ~ 1/6. 0,2 0,2 Lover Bounds on L(ju) in dB 67,96 28.3 1516

b) Bunds on
$$T(5) = \frac{G(5) K(5)}{1 + G(5) K(5)} = \frac{L(5)}{1 + L(5)}$$

If we have an opper bound : $|T(6w)| = \left|\frac{L(6w)}{1 + L(6w)}\right| \leq 6$
Then an equivalent (MMAC) bund on L is:
 $\frac{1}{6} \leq \left|\frac{1 + L(6w)}{L(6w)}\right| = \left|1 + \frac{1}{L(6w)}\right|$
If $\left|\frac{1}{L(6w)}\right| \geq \frac{1}{6} + 1$ then $\left|1 + \frac{1}{L(6w)}\right| \geq \left|\frac{1}{L(6w)}\right| - 1 \geq \frac{1}{6}$
 $\left|\frac{1}{L(6w)}\right| \geq \frac{1}{6} = \frac{1}{6} = \frac{1}{6} |T(6w)| \leq 6$

$$\implies \left| \left| L(y) \right| \leq \frac{b}{b+1} \Rightarrow \left| T(y) \right| \leq b \right|$$

W	upper Bound on IT(1005)	Upper Bound on /L(jw)/	Upper Bound on ILGWII in dB
3	0.3	0,23	-12.7
10	0.04	0,0385	-28,3
100	0,0004	0.0004	-67,96 If the band on
1	I		then the bound on [L(jus)] is a b.

and generated with the second s

Step 2 Use the various design "stages" to get a controller that substies the requirements on [LGw) f. a) G(s) = 10/s First use a proportional gain Kils) = B & Jo that the loop Giss Kilss has the desired cross-over Frequency of we = 1 rad bec. $I = \left| G(jw_c) K_j(jw_c) \right| = \frac{10}{w_c} \cdot \beta \implies \beta = \frac{w_c}{10} = \frac{1}{10}$: Choose Kils) = 1/0 Inchal Loop shope => Lils]= Gls) Kilsi = 1/s 12. (ju) 1 (db) 0 = Lewer bound requirements on /L/ \$80 (derived from 'S requirements) o 68 50 x = Upper bound requirements on IL/ 40 (desived from T requirements) 026 20 06 04 0.2 15-L 10-2 102 10' -12,7 × -20 -28.3 x -40 - [L(S)] -60 - 80 -68 Based on our initial losp shape [Li] we need to increase the low-frequency gain and reduce the high frequency gain. Important Rule of Thumb

- b) We can use either a low frequency boost or integral boost stage to increase the low frequency gain. We'll use a low-frequency boost: $|K_2|$ $K_2(s) = \frac{S+\overline{w}}{S+\overline{w}/S}$
- At $\omega = 0.2$ radface our hopspape has gain $|4.10.2\rangle| = \frac{1}{10.21} = 5$ and the lower bound requirement is $|2.10.2\rangle| \ge 6$. Thus we need the bowt to at least slightly increase the gain at $\omega = 0.2$. Thus we should pick $\omega \ge 0.2$. At $\omega = 10^{-2}$ our loopshape has gain $|2.100.1\rangle| = \frac{1}{0.01} = 100$. The lower bound requirement is $|2.100.1\rangle| \ge 2501$. Thus keeps needs to increase the law frequency gain by $\frac{250}{100} \approx 25$

Mismayo

Our straight -line Bode plots are only rough approximations. I could give you precise formulas for picking $\overline{\omega}$ and β given the specifications above but I think it is easier to iderate with the values. After a few tries I fund the following values are very close to satisfying the regovernents $\overline{\omega} = 0,3$ and $\beta = 50$

dur controller is now $K_1(s) K_2(s) = \frac{1}{10} \frac{S+0.3}{s+0.3/50}$ and the second loopshape is $L_2(s) = G(s) [K_1(s) K_2(s)]$



c) Next we can use a high frequency toll-off to decrease the loop gain at high frequencies so that we are under the upper band specifications. At w=3 md/sec, our second loop-shape has |L2(j3)| = 0.32 and the upper bound requirement is |L2(j3)| ≤ 0.23

Our high - Frequency coll-off his the form Kyls= W

Since we need to decrease the gain at w=3rad/sec we must choose $\overline{w} \leq 3 \operatorname{rad/sec}$. After some trial and error, $\overline{w} = 2.75 \operatorname{rad/sec}$ rem subsfies all design requirements.

